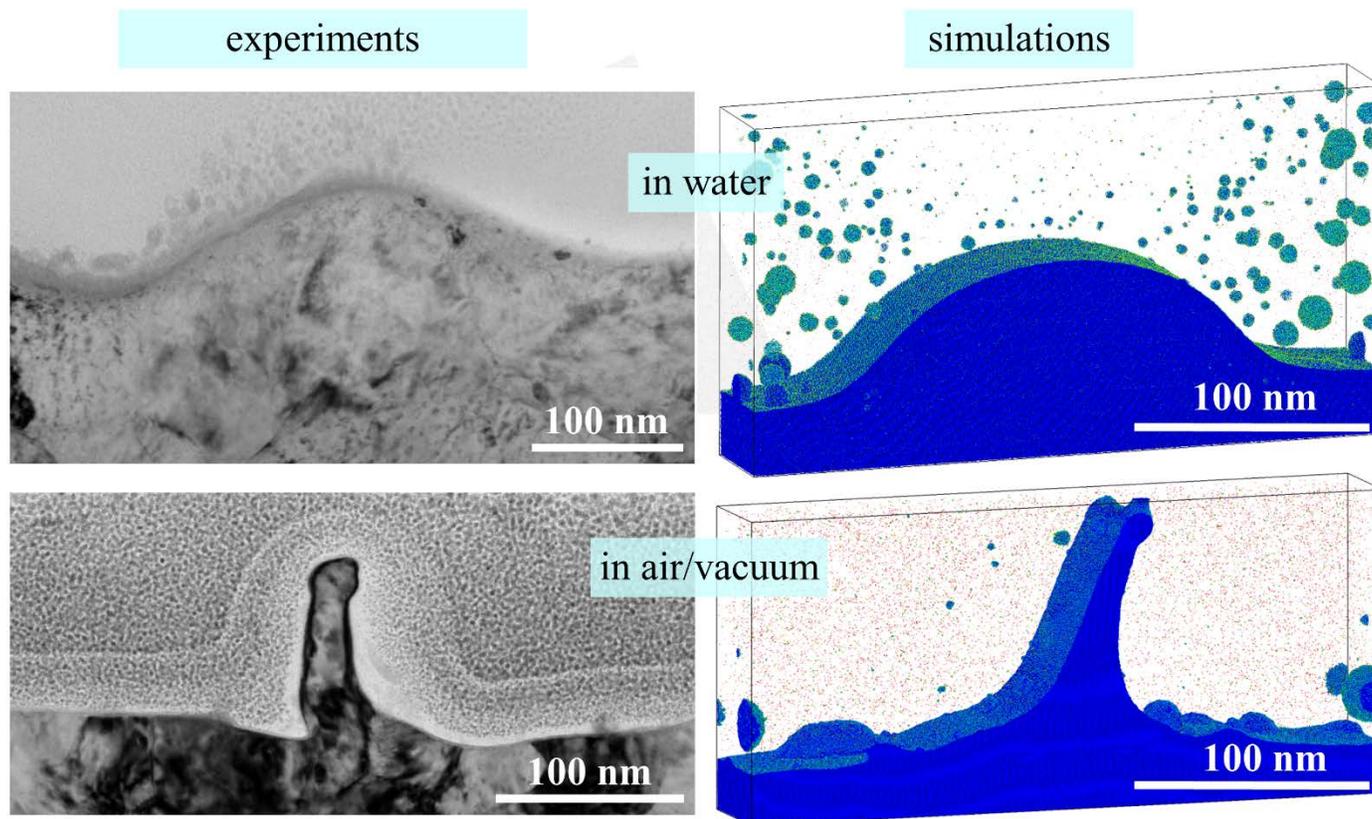


Effect of a liquid environment on single-pulse generation of laser induced periodic surface structures and nanoparticles

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Mechanisms of laser-assisted surface nanostructuring and generation of nanoparticles are revealed in a closely integrated computational and experimental study.

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Effect of a liquid environment on single-pulse generation of laser induced periodic surface structures and nanoparticles†

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The effect of a liquid environment on the fundamental mechanisms of surface nanostructuring and generation of nanoparticles by single pulse laser ablation is investigated in a closely integrated computational and experimental study. A large-scale molecular dynamics simulation of spatially modulated ablation of Cr in water reveals a complex picture of the dynamic interaction between the ablation plume and water. Ablation plume is found to be rapidly decelerated by the water environment, resulting the formation and prompt disintegration of a hot metal layer at the interface between the ablation and water. A major fraction of the ablation plume is laterally redistributed and redeposited back to the target, forming smooth frozen surface features. Good agreement between the shapes of the surface features predicted in the simulation and the ones generated in single pulse laser ablation experiments performed for Cr in water supports the mechanistic insights revealed in the simulation. The results of this study suggest that the presence of a liquid environment can eliminate the sharp features of the surface morphology, reduce the amount of the material removed from the target by more than an order of magnitude, and narrow down the nanoparticle size distribution as compared to laser ablation under vacuum. Moreover, the computational predictions of the effective incorporation of molecules constituting the liquid environment into the surface region of the irradiated target and the generation of high vacancy concentrations, exceeding the equilibrium levels by more than an order of magnitude, suggest a potential for hyperdoping of laser-generated surfaces by solutes present in the liquid environment.

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† Electronic supplementary information (ESI) available: (A) Animated sequences of snapshots from the simulation illustrated in Fig. 2 in the paper; (B) contour plots of density, water concentration, and temperature shown for a time of 100 ps after the laser pulse; (C) contour plots of density, water concentration, and temperature shown for times of 200, 500, and 700 ps; (D) contour plots of density, water concentration, and temperature shown for times of 900, 1200, and 1500 ps; (E) nanoparticle size distributions predicted in simulations of spatially modulated ablation of Cr in water and under vacuum; (F) images of surface features produced in experiments and simulations of single pulse laser ablation of Cr in water and in air/vacuum. See DOI: 10.1039/d0nr00269k

Surface nanostructuring is an effective way to drastically alter the chemical, mechanical, and optical properties of conventional materials and to achieve desired functionality in applications. The deterministic top-down nanofabrication techniques, such as electron or ion beam lithography,^{1,2} scanning probe writing utilizing optical near field effects,^{3,4} or generation of surface features by tightly focused ultrashort laser pulses^{5–7} are all suitable methods for forming high-resolution surface nanostructures. Common shortcomings of these methods, however, are limited scalability and low processing speed, which limit their utilization in industrial applications. A faster surface nanostructuring can be achieved through irradiation with spatially overlapping ultrashort laser pulses, which can yield disordered hierarchical nano/micro-structured surfaces.^{8–12} Moreover, a certain degree of regularity on the laser-processed surfaces can be introduced by spatial modulation of the energy deposition introduced through interference between multiple laser beams^{7,13,14} or naturally occurring interference of the incident laser beam and surface scattered electromagnetic waves,^{15,16} leading to the formation of laser-induced periodic surface structures (LIPSS).^{9–12,16–23}

It has been demonstrated that surfaces subjected to laser nanostructuring can possess unique properties, such as superhydrophobicity and self-cleaning,^{11,17,18} enhanced tribological performance,^{19,20} altered cell adhesion, growth and proliferation,^{21,22} as well as strongly modified optical properties.^{8,17,23} The progress in optimization and tuning of surface structures for practical applications, however, usually involves extensive experimentation with irradiation parameters, such as the laser wavelength, polarization, pulse duration, fluence, repetition rate, scanning speed, and spot diameter. Moreover, since the generation of the surface morphology in laser processing relies, to a large degree, on the spontaneous response of the target material to the rapid laser energy deposition, precise control over the surface structures is not always possible to achieve.

An additional flexibility in tuning the surface morphology can be achieved by performing laser processing in a liquid environment. Indeed, it has been demonstrated in a number of studies that the choice of the liquid can be effectively used to control the microstructure and morphology of laser-treated surfaces,^{24–28,29} which in turn have a strong effect on the ablation rate and nanoparticle production.³⁰ The limited understanding of the fundamental mechanisms responsible for laser-assisted surface nanostructuring in liquids, however, hinders the effective utilization of the opportunities provided by this promising surface processing approach. The theoretical and computational treatments of laser–material interactions in liquids have been largely focused on the generation of nanoparticles^{31–36} and general mechanisms of laser ablation,^{34,37,38} with only a few studies addressing the effect of the liquid environment on generation of surface structures and subsurface defects.^{14,34,39} In particular, recent molecular dynamics (MD) simulations of the laser interaction with a Ag target in water have revealed the ability of the liquid environment to suppress the nucleation of subsurface voids and facilitate the formation of a nanocrystalline surface structure upon melting and resolidification.³⁹ At higher fluences, the water environment has been shown to help stabilize large subsurface voids leading to surface swelling,³⁴ whereas a thin liquid overlayer has been shown to partially suppress localized spallation from a Au target.¹⁴

In this article, we address the general question on the fundamental mechanisms responsible for laser-assisted surface nanostructuring in liquids by performing a closely integrated computational and experimental study of the generation of LIPSS in the ablative regime. The recent demonstration of the formation of highly regular LIPSS by a nearly single pulse irradiation at laser fluences significantly above the ablation threshold^{40,41} not only suggests a viable surface processing technique capable of competing with current industrial surface processing methods^{42,43} but also provides an opportunity to directly probe the effect of the liquid environment on the laser-generated surface morphology under well-controlled single pulse irradiation conditions. The process of spatially modulated ablation of a Cr target in water is studied here in a large-scale MD simulation and in experiments performed

under similar irradiation conditions. The simulation reveals a complex picture of the dynamic interaction between the ablation plume and water, which has a dramatic effect on the lateral redistribution of the material and drastically alters the final shape of the surface structures in comparison with earlier results obtained under vacuum.⁴⁴ The shapes of the surface structures observed in the experimental study of the single pulse LIPSS formation on a Cr surface irradiated in air and water environments are in good agreement with the predictions of the atomistic modeling, thus supporting the mechanistic insights obtained from the simulations.

Results and discussion

The simulation and experiments reported in this paper are performed for a bulk single crystal Cr target with a (100) surface orientation irradiated with a single 200 fs laser pulse. The incident fluence of 6000 J m^{-2} used in experiments performed in air is well above the ablation threshold and corresponds to irradiation conditions where the formation of highly regular LIPSS is observed in surface processing by weakly overlapping laser pulses.^{40,41} As can be seen from Fig. 1a–c, which show the surface morphology produced in the central part of the laser spot, even a single pulse laser irradiation in this regime is capable of causing significant material redistribution and generation of surface patterns that serve as precursors for the formation of well-developed LIPSS upon surface scanning by overlapping laser pulses. The SEM image in Fig. 1a reveals a sequence of parallel lines with noticeable periodicity, while an enlarged view of one of the lines provided in Fig. 1b and a TEM image of a thin slice (lamella) extracted by FIB milling from a small region that cuts through one of these lines, shown in Fig. 1c, expose a relatively sharp shape of the surface protrusion, with its height significantly exceeding its width. Since the spot illustrated in Fig. 1a–c is irradiated with a single laser pulse, the produced quasi-periodic surface morphology is not defined by any preexisting periodic motif and clearly demonstrates the generation of LIPSS-like structures in a single pulse irradiation regime.

The incident laser fluence of 6000 J m^{-2} can be converted to the absorbed fluence of 2200 J m^{-2} by assuming a constant value of reflectivity of 0.63 for a wavelength of 1026 nm (ref. 45) used in the experiment. This assumption can be justified by the relatively small (less than 10%) variation of the reflectivity in a range of electron temperatures from zero to 25 000 K predicted from *ab initio* simulations for Cr at a laser wavelength of 1030 nm.⁴⁶ A recent large-scale atomistic simulation of spatially modulated ablation under vacuum⁴⁴ performed in a similar irradiation regime (20% modulation around an average level of 2500 J m^{-2}) has revealed a complex dynamic picture of material removal and redistribution leading to the formation of prominent surface features extending above the level of the original surface of the irradiated target. Lateral pressure gradients in the plume generated by the spatially modulated laser ablation drive the vapor and liquid droplets to

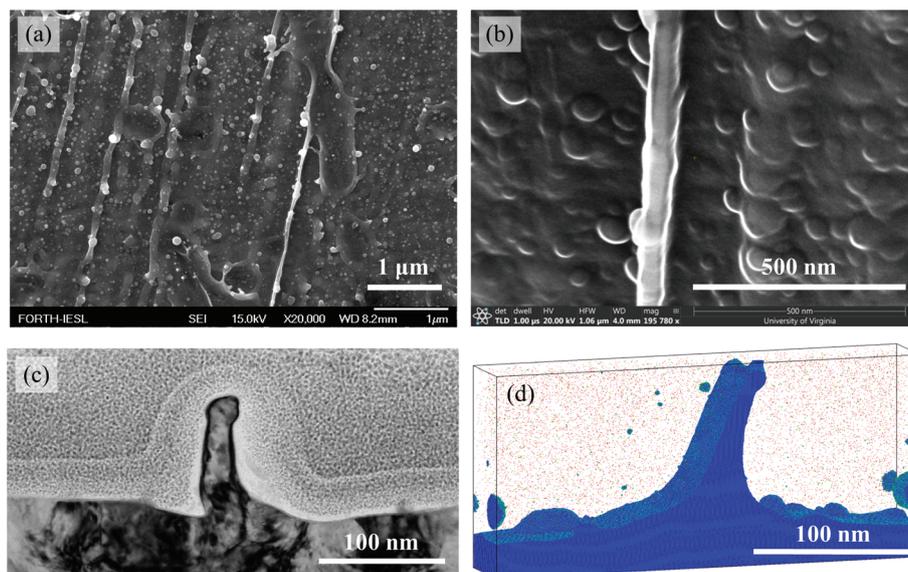


Fig. 1 Surface morphology generated on a Cr (001) target irradiated *in air* with a single 200 fs laser pulse at an incident laser fluence of 6000 J m^{-2} and illustrated here by two SEM images of the surface (a and b) and a TEM image of a cross-sectional slice extracted from a surface area that includes a protrusion generated by the laser irradiation (c). The shape of the surface protrusion in (c) can be related to the shape of a frozen surface feature obtained in a large-scale MD simulation of spatially modulated laser ablation of the Cr (001) target performed under vacuum and irradiation conditions similar to those used in the experiment (d).

the regions located above the minima of the laser energy deposition at the target surface. The material redistribution leads to the formation of a transient elongated liquid wall extending up to $\sim 600 \text{ nm}$ above the surface of the target. The upper part of the liquid wall disintegrates into droplets, while the base of the wall evolves into a relatively sharp protrusion captured by solidification on a time scale of $\sim 2 \text{ ns}$. The final height, thickness, and shape of the surface protrusion predicted in the simulation and shown in Fig. 1d are strikingly similar to those of the surface feature observed in the TEM image in Fig. 1c. Moreover, a frozen liquid droplet at the top of the simulated surface protrusion is also present in the TEM image in Fig. 1c, thus supporting the mechanism of the ablative generation of LIPSS through disintegration of a transient liquid wall suggested by the simulation. Note that earlier simulations performed under a 1 atm Ar atmosphere^{47,48} demonstrate that, while the presence of atmospheric background gas pressure affects the evolution of ablation plume and nanoparticle generation, it has no influence on the flow of the molten material in the vicinity of the target surface and the final morphology of the solidified target. This observation justifies the direct comparison of the surface morphology predicted in the simulation performed under vacuum (Fig. 1d) with experimental results obtained in air (Fig. 1c).

To investigate the effect of the liquid environment on the laser-assisted surface nanostructuring, we performed a large-scale MD simulation of the single-pulse LIPSS formation in water under irradiation conditions similar to those used under vacuum (see Methods for the model description). The presence of the liquid environment above the Cr target drastically changes the dynamics of ablation plume expansion, as can be

seen from atomistic snapshots shown in Fig. 2 and the fields of density, concentration of water, and temperature shown in Fig. 3. Instead of the free expansion and lateral redistribution of the ablation plume observed under vacuum,⁴⁴ the hot mixture of vapor and liquid droplets produced in the explosive decomposition of the superheated Cr target is rapidly decelerated by the water environment and remains confined within just an $\sim 150 \text{ nm}$ region above the irradiated surface. The top part of the ablation plume comes in direct contact with water and produces a narrow region where water superheated above its critical temperature is mixed with the Cr vapor. This narrow mixing region shows up at 100 ps as a thin green stripe in a plot of water concentration shown in Fig. 3. The Cr atoms in this region are rapidly quenched and condense into a nanogranular layer composed of atomic clusters and nanoparticles, which is apparent from the atomistic snapshots and density plots shown for 100 and 200 ps in Fig. 2 and 3.

The initial upward motion of the ablation plume rapidly slows down and turns back within just 200 ps after the laser irradiation, as can be seen from the local momentum density (defined as a product of the local velocity and mass density) vectors plotted on the density fields in Fig. 3. At 200 ps, the relatively dense layer of Cr formed at the interface with water still moves upwards, while the lower part of the plume is already reflected from the interface and moves down. Meanwhile, the pressure created by superheated water in the mixing region pushes the interfacial region down and, by the time of 500 ps, the Cr nanoparticles formed by decomposition of the interfacial layer are already entrained into the hot supercritical water expanding towards the target surface.

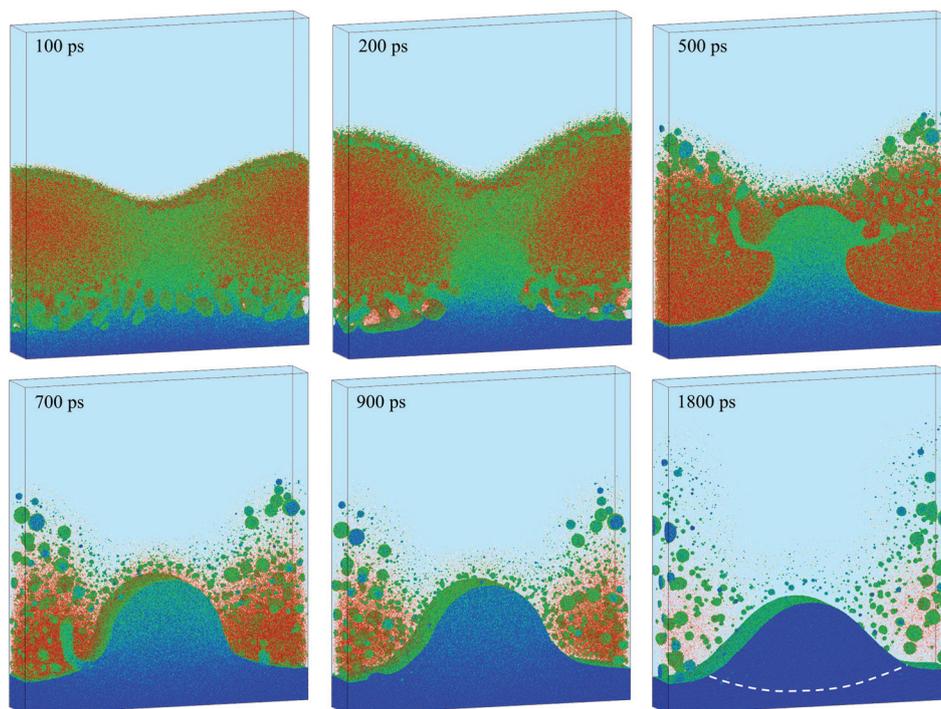


Fig. 2 Snapshots of atomic configurations predicted in a simulation of a bulk Cr target irradiated *in water* with a 200 fs laser pulse at an average absorbed fluence of 2500 J m^{-2} with 20% of energy modulation. Only parts of the computational system from 60 nm below the initial surface of the Cr target up to 240 nm above the surface are shown in the snapshots. The atoms are colored according to their potential energies, from blue for molten Cr to red for vapor-phase Cr atoms. The molecules representing the water environment are not shown, and the presence of water is illustrated schematically by a light blue region above the Cr target. The white dashed line in the snapshot shown for 1800 ps marks the location of the solidification front. An animated sequence of snapshots from this simulation can be found in the ESI.†

The processes of plume reflection and redeposition proceed simultaneously with lateral material redistribution driven by strong pressure gradients generated in the course of spatially modulated ablation and directed towards the central part of the computational system, *i.e.*, the region located above the part of the target surface that received the minimum of the laser energy deposition. The pressure gradients drive the collective motion of Cr vapor and liquid droplets towards the center, as can be seen from the momentum density vectors in the ablation plume. The vectors have components directed towards the center both at the stage of the initial plume expansion and upon its reflection from the water environment, as can be seen from the density plots shown in Fig. 3 for 100 and 200 ps, respectively. While at 100 ps the densest part of the ablation plume appears to be weakly connected to the target by a porous/foamy region, the lateral pressure gradients and material redistribution quickly compact this region, leading to the formation of a thick “wall” with continuous density distribution. In contrast to the spatially modulated ablation under vacuum, where the lateral material redistribution leads to the formation of an elongated thin liquid wall rapidly expanding in the vertical direction,⁴⁴ the presence of the water environment suppresses the upward expansion of the plume and results in splashing of the top part of the wall into a wing-like transient structure seen at 500 ps in Fig. 2 and 3.

The subsequent evolution of the shape of the liquid wall is strongly affected by the complete disintegration of the transient

layer generated at the initial stage of the ablation process through accumulation of the ablation plume at the interface with water. The disintegration of the layer into individual nanoparticles occurs by ~ 500 ps and lets the supercritical water to stream towards the surface of the target, as can be seen from plots of water concentration shown in Fig. 3 for 500 and 900 ps, and in the ESI† for 700 ps. The water entrains the Cr nanoparticles, pushes the “wings” of the liquid wall/bump down, and contributes towards smoothing the overall shape of the bump.

The mixing of water with the hot ablation plume (Cr vapor and small clusters) confined near the surface of the target by the water environment results in a fast quenching of the plume and massive nucleation and growth of Cr nanoparticles. This process is reflected in the decrease in the density of vapor-phase Cr atoms (red dots in Fig. 2) as time progresses from 500 to 700 to 900 and to 1800 ps in Fig. 2, as well as in the rapid cooling seen in the sequence of temperature profiles shown in Fig. 3. While some of the nanoparticles are redeposited to the target, many are entrained into vortices that develop in the vapor cavity as the supercritical water flows along the semi-spherical bump of molten Cr. The streams of hot water and nanoparticles collide within the peripheral area and induce an upward motion of vapor and nanoparticles, as can be seen from the momentum density arrows in the density plots shown in Fig. 3 for 900 and 1500 ps, and in the ESI† for 700 and 1200 ps. This motion leads to the expansion of the low-density

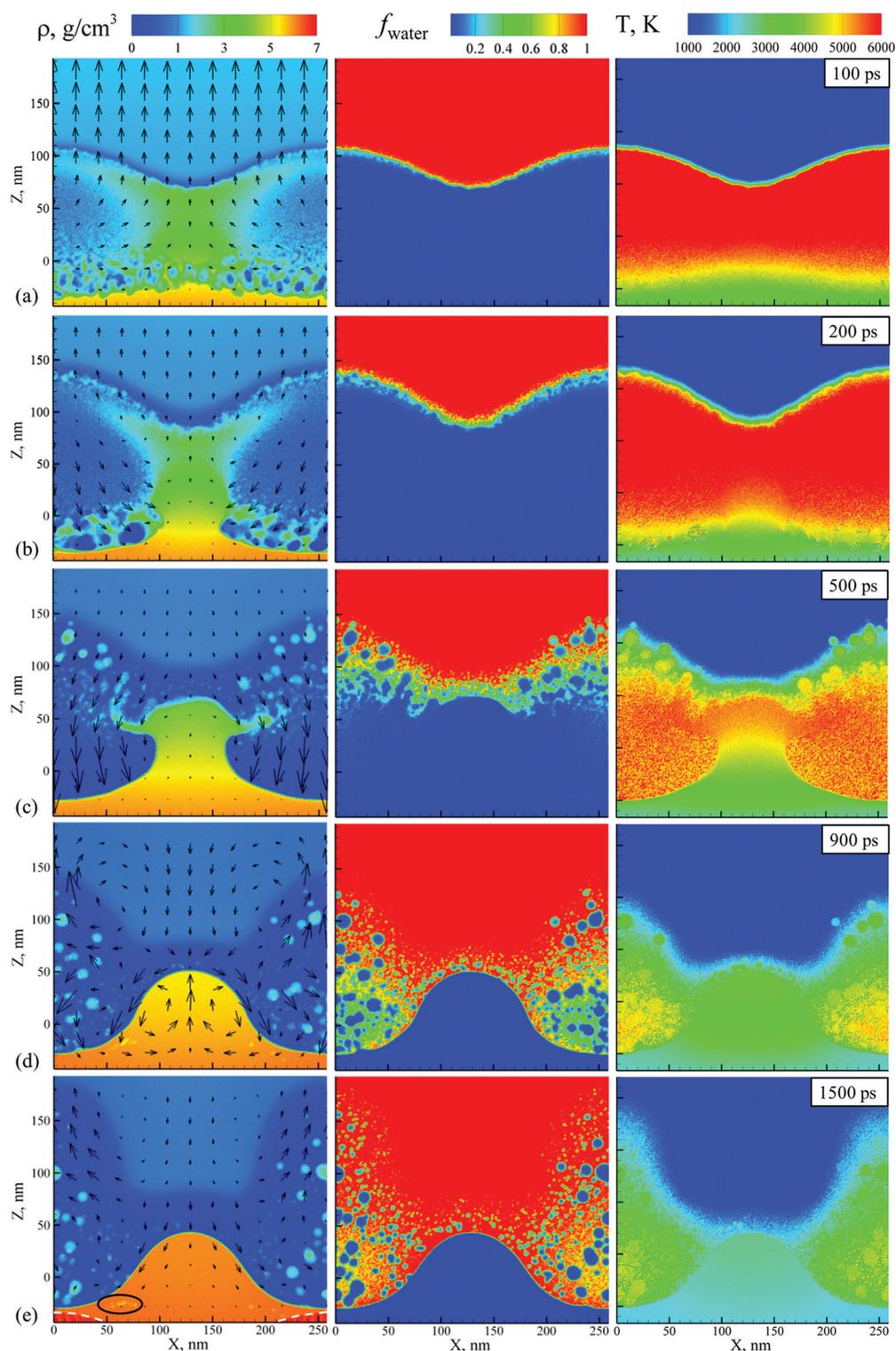


Fig. 3 Contour plots of density, water concentration, and temperature shown for different times in the simulation of spatially modulated ablation of Cr in water illustrated in Fig. 2. The arrows in the density plots indicate the direction and the relative magnitude of the local momentum density. The length of the vectors is scaled up with respect to the ones shown for 100 ps by a factor of 1.67 in plots shown for 200 and 500 ps and by a factor of 13.3 in plots shown for 900 and 1500 ps. Only parts of the computational system from -43 nm to 193 nm with respect to the initial surface of the Cr target are shown. Black ellipse in the density plot shown for 1500 ps outlines a region with several water nanobubbles captured during plume redeposition. White dashed lines in the same plot show the location of the solidification front. Additional contour plots for times 700 and 1200 ps are provided in the ESI.†

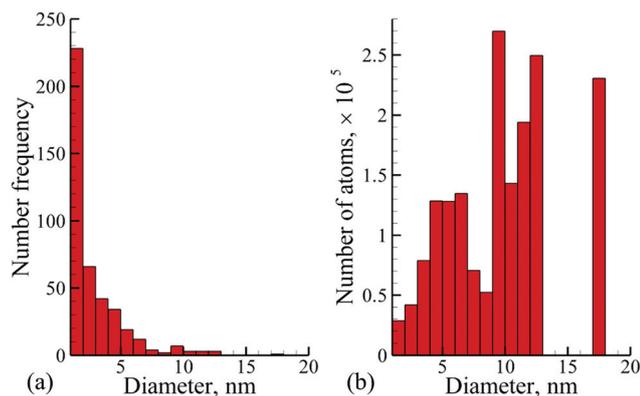


Fig. 4 Nanoparticle size distribution predicted in the simulation of spatially modulated ablation of Cr in water illustrated in Fig. 2. The distribution is shown for a time of 2.2 ns after the laser pulse. The number of nanoparticles of different sizes and the total number of atoms in the nanoparticles of the corresponding sizes are shown in (a) and (b), respectively. Atomic clusters with equivalent diameters smaller than 1 nm are not included in the distributions.

hot region where the ablation plume is mixed with supercritical water. This mixing region can be considered to be a precursor of the cavitation bubble typically observed in time-resolved experimental probing of pulsed laser ablation in liquids.^{49–51}

Many of the nanoparticles present in the mixing region at the initial stage of the cavitation bubble expansion studied in the simulation can be expected to end up in the water environment upon bubble collapse, forming a colloidal solution. The cluster analysis performed for an atomistic configuration produced by the end of the simulation at 2.2 ns, Fig. 4, reveals a broad distribution of nanoparticle diameters ranging from 1 to 18 nm. While the nanoparticle size distribution shown in Fig. 4 is likely to undergo further changes during the cavitation bubble expansion and collapse, it still provides an important insight into the origin of the final broad or even bimodal nanoparticle size distribution commonly observed in experimental studies of nanoparticle generation by laser ablation in liquids.^{35,52,53} Moreover, recent time-resolved X-ray probing of the cavitation bubbles⁵¹ indicates that large nanoparticles appear early in the ablation process and are present already at the advancing fronts of the expanding bubbles. These results suggest that the processes occurring at the initial stage of the ablation process are likely to play the key role in defining the final nanoparticle size distribution.

The majority of nanoparticles generated in the simulation are small, below 5 nm in diameter (Fig. 4a), and are formed through rapid nucleation and growth in the region where the Cr plume is quenched as a result of mixing with water. At the same time, most of the Cr material removed from the target is present in much less numerous larger nanoparticles with a diameter above 10 nm, as can be seen from Fig. 4b, where the distribution is shown in terms of the number of atoms in nanoparticles of different sizes. As discussed above, these large nanoparticles originate from decomposition of the transient dense and hot Cr layer formed at the interface with the

water environment. The generation of large nanoparticles in the course of decomposition of a dense layer formed at the metal–water interface has been observed in earlier MD simulations performed under conditions of spatially homogeneous laser energy deposition for thin Ag films³³ and bulk targets.^{34–36} In these simulations, the layer roughening and disintegration were found to be facilitated by the Rayleigh–Taylor instability of the interface between the higher density metal layer decelerated by the pressure from the lighter supercritical water. In the case of the spatial modulation of laser energy deposition investigated in the present work, the lateral pressure gradients and the corresponding material redistribution in the ablation plume serve as a major additional factor leading to the rapid disintegration of the interfacial layer into nanoparticles. The prompt layer disintegration also prevents the formation of the largest nanoparticles that emerge from the much slower evolution and fragmentation of the flat dense layer occurring in the absence of the lateral disturbances. The computational prediction on the elimination of the largest nanoparticles in the spatially modulated ablation suggests a possible approach for minimization of the material waste in nanoparticle generation by laser ablation in liquids, which is of particular importance for precious metals.

By turning our attention from the nanoparticle generation to the evolution of the surface morphology, we observe gradual smoothing of the shape of a surface bump generated by the lateral material redistribution and redeposition at the initial stage of the ablation process (*cf.* images for times after 700 ps in Fig. 2 and 3). The smoothing of the bump is largely driven by surface tension and proceeds simultaneously with cooling and epitaxial regrowth of the crystalline target. The location of the advancing solidification front is marked by white dashed curves for times of 1.5 and 1.8 ns in Fig. 3e and 2, respectively. The rapid advancement of the solidification front results in complete solidification of the bump by ~ 2.2 ns. The final shape of the frozen surface features a smooth hemicylindrical bump that rises ~ 65 nm above the lowest levels of the new surface in the valleys adjacent to the bump. This shape is very different from the one predicted in the simulation performed for the same irradiation conditions under vacuum, where the formation of an elongated protrusion with the height exceeding 100 nm is observed, Fig. 1d.

In addition to the distinct shapes of the surface protrusions formed in the single pulse spatially modulated laser ablation in water and under vacuum, the environment strongly affects the total amount of the material removed from the target. The ablation yield in the simulation performed under vacuum is 22 868 721 atoms, which corresponds to the 24.6 nm-deep surface layer in the initial crystalline Cr target. The total amount of Cr that ends up mixed with supercritical water in the slowly expanding cavitation bubble is more than an order of magnitude lower, 1 764 198 Cr atoms, which corresponds to an equivalent 1.9 nm-thick layer of the initial target. The drastic drop of the ablation yield in the presence of the water environment can be explained by the reflection of a major fraction of the ablation plume from the water–plume interface and redeposition of the

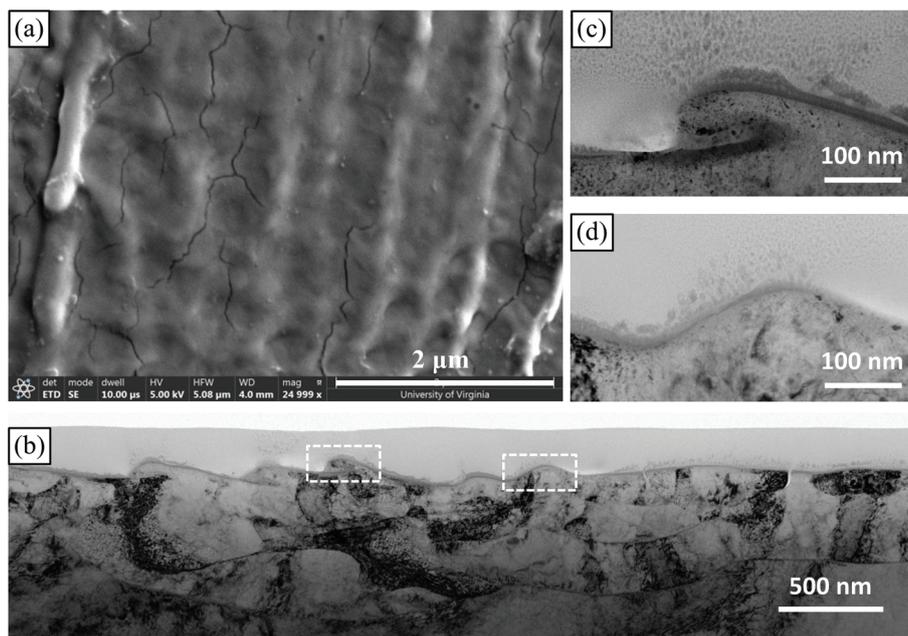


Fig. 5 Surface morphology generated on a Cr (001) target irradiated *in water* with a single 200 fs laser pulse at an incident laser fluence of 6000 J m^{-2} and illustrated here by an SEM image of the surface (a) and a TEM image of a cross-sectional slice extracted from the laser spot (b). Enlarged views of two regions outlined by dashed rectangles in (b) are shown in (c) and (d).

material to the target. One implication of this observation is that surface processing in a liquid environment is much more sparing in terms of the material waste, and may be preferable in applications where surface recession should be avoided and/or the ejection of ablation products presents a health hazard.

In order to verify the computational predictions on the strong effect of the liquid environment on the morphology of the laser-processed surface, the experimental study of the ablative surface modification in air, discussed above and illustrated in Fig. 1a–c, is extended to laser processing in water. Except for the environment, all other experimental conditions are kept the same, *i.e.*, single pulse irradiation of a single crystal Cr (100) surface at a wavelength of 1026 nm and an incident fluence of 6000 J m^{-2} . The surface morphology is characterized by SEM imaging and TEM analysis of a cross-sectional slice extracted from the laser spot, Fig. 5. As can be seen from the SEM image of a surface region located near the center of the laser spot, Fig. 5a, one of the most notable effects of the presence of the water environment is the pronounced smoothing of the surface morphology, as compared to the one generated by ablation in air, Fig. 1a. This observation agrees well with the results of the atomistic simulations that predict the formation of much smoother surface features in water as compared to vacuum conditions (*cf.* Fig. 1d and the last panel in Fig. 2).

The spatial period of LIPSS produced in the experiment conducted in water is approximately 500 nm, which is consistent with prior studies of LIPSS formation in the water environment showing a much shorter period of surface structures than the laser wavelength, in contrast to the LIPSS formation

under vacuum.^{54,55} The typical elevation of the smooth bumps is $\sim 100 \text{ nm}$, as illustrated by the TEM image of a cross-section cutting through several surface features shown in Fig. 5b. Some of these features are remarkably similar to the ones obtained in the simulation, *cf.* Fig. 5d and the last panel in Fig. 2. Other features, such as the one shown in Fig. 5c, have shapes resembling frozen nano-waves. These unusual shapes can be attributed to uneven distribution of the laser energy deposition within the laser spot. In addition to the periodic absorption pattern created by the interference of the incident and surface scattered electromagnetic waves,^{15,16} the Gaussian shape of the laser energy deposition profile leads to the emergence of global pressure gradients in the ablation plume confined by water. This pressure gradient is directed from the center to the periphery of the laser spot and is likely to be responsible for splashing the surface features in this direction, as can be seen in Fig. 5b and c.

The observation that frozen surface features generated in the simulation (Fig. 2) and experiment (Fig. 5d) not only have similar shapes but similar dimensions (height and width) as well is surprising, as the length-scale of the modulation of the laser energy deposition is substantially larger in experiment as compared to that in the simulation. This striking quantitative match of the dimensions of the laser-generated surface features suggests that, while the periodicity of ablative LIPSS is largely controlled by the laser wavelength, the shape and dimensions of the surface features are less sensitive to the laser wavelength and are defined by the ablation depth and the dynamics of the interaction of the ablation plume with the water environment.

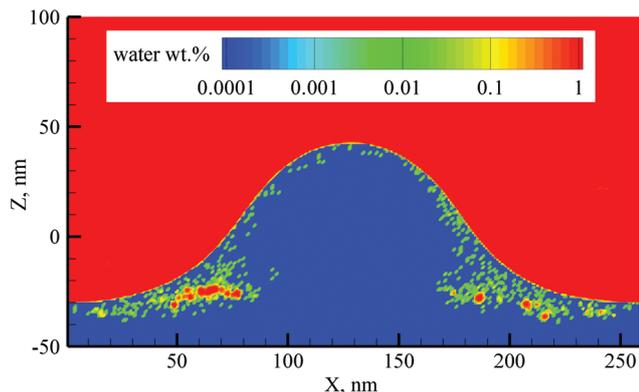


Fig. 6 Contour plot of the water concentration in the surface bump generated in the simulation illustrated in Fig. 2 and 3 by the time of 1500 ps, when the bump is still in the molten state. The contour plot is shown on the logarithmic scale that reveals the incorporation of water into the surface layer of the bump. The water molecules and nanobubbles at the base of the bump are trapped by the rapid solidification process, suggesting that laser processing in liquids can be used as a method to achieve hyperdoping of the surface region of the irradiated target by molecules present in the liquid environment.

The good agreement between modeling and experiments in the effect of the water environment on the surface morphology produced by single pulse laser ablation provides strong support to the notion that the mechanisms revealed in the simulations reflect the reality. It also encourages further analysis of laser-generated surface features aimed at exposing the details of the nanostructure that is difficult to probe experimentally. One finding from the analysis of the microstructure of the resolidified surface bump is that a substantial number of molecules constituting the liquid environment is incorporated into the bump, as can be seen from the water density contour plot shown in Fig. 6. Water is mainly present near the base of the bump, where clusters of nanobubbles filled with water are generated at the early stage of the bump formation, when the ablation plume is reflected from the water environment and redeposited to the target. The nanoscale water bubbles can also be clearly seen in Fig. 7c, where both external and internal surfaces are shown by gray color, as well as in the density contour plots, *e.g.*, in a region outlined by the solid oval in Fig. 3e. Water is also present throughout the surface region of the target, where it is more evenly distributed with the average water concentration in a 10 nm-thick surface layer of 0.017 wt%. The effective incorporation of molecules constituting the liquid environment into the surface region of the irradiated target suggests a potential for hyperdoping (*i.e.*, doping far beyond the material solubility limit) of laser-generated surface features by the liquid molecules or solutes present in the liquid environment. Indeed, the doping of oxide nanoparticles⁵⁶ and Si surface structures^{57,58} generated by laser ablation in liquids by elements added to the liquid environment has recently been demonstrated experimentally.

The penetration of the solute deeper into the target may be facilitated by the vortices transiently appearing in the molten

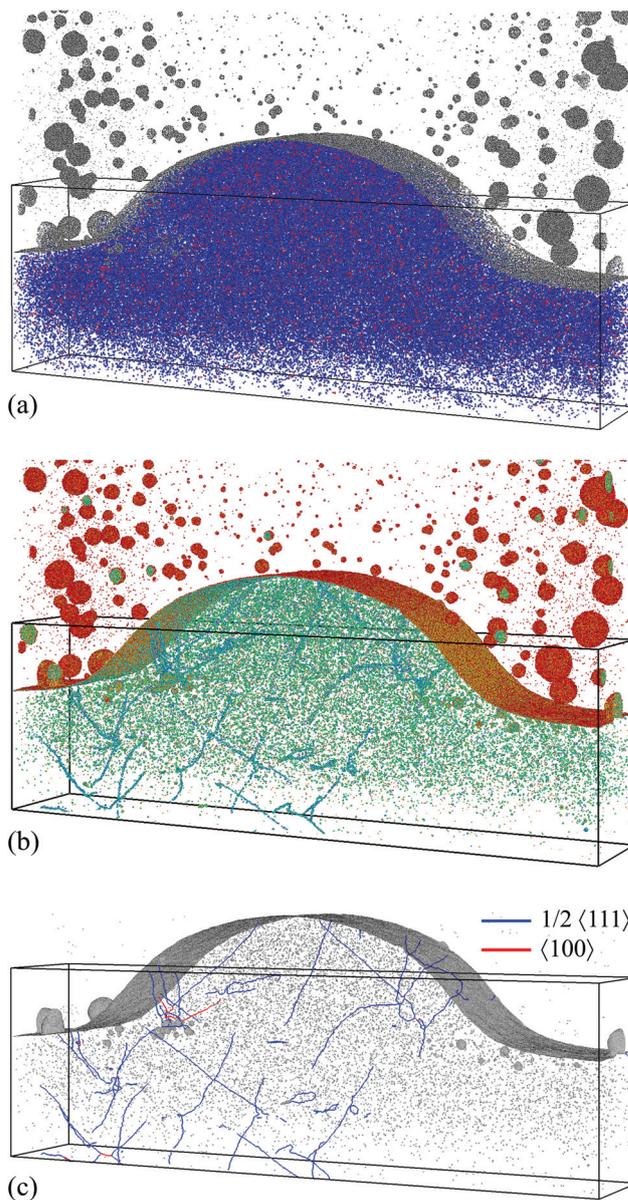


Fig. 7 Three representations of the microstructure of the surface region of the irradiated Cr target at 2200 ps, after complete resolidification of the target. In (a), the atoms surrounding vacancies and divacancies are shown by blue and red color, respectively. In (b), dislocations and vacancy clusters present in and below the frozen bump are exposed by blanking the atoms with the potential energy below -3.94 eV (corresponding to atoms with bcc local coordination and atoms surrounding single vacancies), and the remaining atoms are colored according to their potential energy with the color scale ranging from -4.0 eV (blue) to -3.4 eV (red). In (c), dislocations identified with the algorithm described in ref. 61 are shown and colored according to the dislocation type. Gray color in this panel outlines the free surface of the Cr target, clusters of vacancies (gray dots), and surfaces of voids (gray three-dimensional shapes inside the bump) formed as a result of entrapment of water vapor during plume redeposition. The rectangular box outlines the shape of the original target before the laser irradiation. Before the structural analysis, the system is quenched for 1 ps using the velocity damping technique.

bump structure and illustrated by arrows in the density plot shown for 900 ps in Fig. 3d, as well as by the long-term solid-state diffusion in the resolidified surface region. The latter can be enhanced by the strong vacancy supersaturation generated in the course of laser-induced melting and resolidification. The distribution of vacancies and divacancies is shown in Fig. 7a, while the larger vacancy clusters can be seen in Fig. 7b, where the atoms with low potential energies are blanked, so that the dislocation cores and vacancy clusters are exposed. The average concentration of vacancies and divacancies within the surface bump is 0.218% and 0.0113%, respectively. This level of vacancy concentration is significantly above the equilibrium vacancy concentration at the final temperature of the bump, but is similar to the vacancy concentration observed in earlier atomistic simulations of laser processing of Cr targets under vacuum.^{44,59} The generation of strong vacancy supersaturation is attributed to the rapid propagation of the solidification front proceeding under conditions of strong undercooling below the equilibrium melting temperature, which has been shown to produce high vacancy concentrations.⁶⁰ The rapid solidification process also results in the formation of a network of dislocations. The dislocation configurations can be identified in Fig. 7b, where the chains of atoms with elevated potential energy correspond to dislocation cores, as well as in Fig. 7c, where the dislocation lines are identified by the dislocation extraction algorithm described in ref. 61. Similar to the surface features generated by spatially modulated ablation under vacuum,⁴⁴ the dislocation network consists of dislocations with a Burgers vector of $a/2 \langle 111 \rangle$ connected by several segments of $a \langle 100 \rangle$ dislocations, where a is the bcc lattice parameter of Cr. The average dislocation density within the surface bump is $\sim 10^{15} \text{ m}^{-2}$.

Summary

The fundamental mechanisms responsible for femtosecond laser induced surface nanostructuring and generation of nanoparticles by laser ablation in a liquid environment are investigated in a joint computational and experimental study performed for a bulk single crystal Cr target irradiated with a single laser pulse in the regime of ablative LIPSS formation. A large-scale MD simulation of spatially modulated ablation of Cr in water reveals a complex picture of the dynamic interaction of the ablation plume with water, which has a dramatic effect on the lateral redistribution of the material and the final shape of the surface structures. Similar to the irradiation under vacuum, laser excitation and fast electron–phonon thermalization of the deposited energy lead to the rapid melting, superheating, and explosive decomposition of the top ~ 40 nm surface layer of the Cr target into a mixture of vapor and liquid droplets (the process commonly referred to as phase explosion). Instead of the free expansion of the ablation plume observed under vacuum, however, the hot mixture of vapor and liquid droplets is rapidly decelerated by the water environment. Water in contact with the ablation plume is heated well

above its critical point, and its expansion pushes the hot metal layer accumulated at the interface between water and the ablation plume back, toward the target surface, leading to redeposition of a major part of the plume.

The processes of plume reflection and redeposition proceed simultaneously with lateral material redistribution driven by pressure gradients generated in the course of spatially modulated ablation and directed towards the region at the minimum of the laser energy deposition. The lateral material redistribution and the vertical confinement of the plume by the water environment result in the formation of a thick wall-like structure that gradually evolves into a liquid bump with a smooth shape and continuous density distribution. This evolution from the wall-like structure into a smooth bump is driven by the surface tension and is assisted by the rupture and disintegration of the interfacial layer of the hot molten metal generated at the water–plume interface, which allows the supercritical water to stream towards the surface of the target and to smooth-out the shape of the bump. The epitaxial regrowth of the crystalline part of the target results in complete solidification of an ~ 65 nm-tall bump by ~ 2.2 ns after the laser pulse. The final shape of the bump predicted in the simulation is remarkably similar to the one revealed in the TEM analysis of the surface morphology generated in the single pulse laser ablation experiments performed in water. The good agreement between modeling and experiments provides strong support for the mechanistic insights obtained from the simulation and described above. It also suggests that, in contrast to the periodicity of ablative LIPSS that scales with the laser wavelength, the shape and dimensions of the laser-generated surface features are less sensitive to the laser wavelength and are largely defined by the ablation depth and the dynamics of the interaction of the ablation plume with the water environment.

The results of the atomistic modeling reported in this paper not only provide insights into the complex dynamic processes involved in spatially modulated laser ablation in liquids, but also reveal several general aspects of these processes that may have important practical implications. The first and most apparent conclusion of this study is that the presence of the liquid environment tends to eliminate the sharp features of the surface morphology produced in laser processing, thus suggesting that the liquid environment is an effective experimental parameter to engineer the shape of LIPSS and other related nanostructures. Second, the total amount of material removed from the target and converted into colloidal nanoparticles is more than an order of magnitude lower in laser ablation in water as compared to the ablation yield predicted for similar irradiation conditions under vacuum. This observation suggests that surface nanostructuring in liquids may be preferable in applications where surface recession should be avoided and/or the ejection of ablation products present a health hazard. Third, the effective incorporation of molecules constituting the liquid environment into the surface region of the irradiated target, as well as the generation of strong vacancy supersaturation in the bump struc-

ture, predicted in the simulation, suggests a potential for hyperdoping of laser-generated surface features by solutes present in the liquid environment. Finally, the computational prediction of the prompt disintegration of the interfacial layer into nanoparticles assisted by the lateral pressure gradients suggests the spatially modulated ablation as an effective method for elimination of largest nanoparticles and minimization of the material waste in nanoparticle generation by laser ablation in liquids.

Methods

Computational model

The simulation reported in this paper is performed for a bulk Cr target covered by water and irradiated with a femtosecond laser pulse with a spatially modulated laser energy deposition. A hybrid computational model^{62,63} combining a continuum level description of laser excitation of electrons followed by electron–phonon equilibration based on a two temperature model⁶⁴ (TTM), a classical atomistic MD representation of the response of the Cr target to the fast laser energy deposition, and a coarse-grained (CG) MD representation of the liquid environment parametrized for water is used in the simulation. The CG MD model combines the breathing sphere model developed for simulations of laser interactions with molecular systems⁶⁵ with a heat bath approach that associates an internal energy variable with each coarse-grained particle.^{33,34,66,67}

A schematic representation of the computational system is shown in Fig. 8. The initial dimensions of the TTM-MD domain representing the Cr target are 260 nm × 43 nm × 140 nm, which correspond to 131 million Cr atoms. The Cr target has a bcc crystal structure and a (001) surface orientation. The periodic boundary conditions are applied in the lateral directions, parallel to the surface of the target. The interatomic interactions are described by the embedded atom method (EAM) potential parametrized for Cr.⁵⁹ The electronic heat transfer in the deeper part of the target, where no structural changes are expected, is described based on the conventional TTM approach. The depth covered by the TTM is chosen to be 2.5 μm to ensure a negligible temperature change at the bottom of the computational system by the end of the simulation.

Above the bulk Cr target, the water environment is represented by a 300 nm-thick layer of CG MD (37.4 million CG particles) covered by dynamic acoustic impedance matching boundary conditions based on an imaginary plane approach described in ref. 68 (denoted as a nonreflecting boundary, NRB in Fig. 8). The cross-interaction between Cr and CG water is described with LJ potential with the energy parameter ϵ fitted to the experimental values of Cr–water interfacial energy^{69,70} and the length parameter σ taken as the average of the equilibrium distances between CG water particles and EAM Cr. At the bottom of the TTM-MD part of the model, a recently developed Langevin nonreflecting boundary (LNRB) condition⁴⁴ is applied. This boundary condition

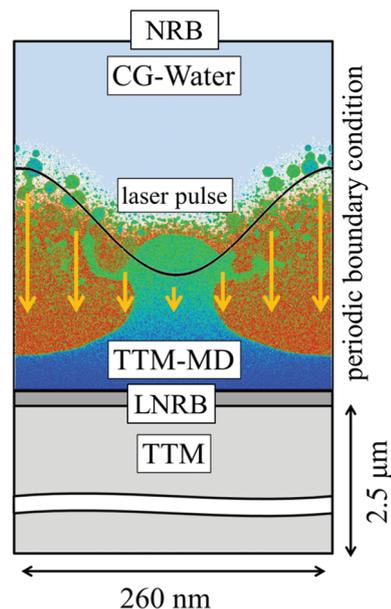


Fig. 8 Schematic representation of the computational setup used in the simulation of single pulse ablative LIPSS formation in water environment. An atomistic snapshot from the simulation at 500 ps after the laser irradiation is used as the background in the representation of the atomistic (TTM-MD) part of the model. Only parts of the computational system from -60 nm with respect to the initial surface of the Cr target are shown in the snapshot. The atoms are colored according to their potential energies, from blue for molten Cr to red for vapor-phase Cr atoms. The molecules representing the water environment are blanked, and the presence of water is illustrated schematically by a light blue region labeled as CG-water. The black curve shows schematically the modulation of the laser energy deposition along the x -direction. The continuum part of the model, and dimensions of the atomistic and continuum regions are not drawn to scale.

ensures nonreflective propagation of the laser-induced pressure waves even in the case of non-planar waves generated in spatially modulated laser ablation. The application of NRB and LNRB enables an adequate representation of experimental conditions in laser ablation of a bulk target covered by a thick liquid layer, where the reflections of the pressure waves from the back surface of the irradiated target and the outer surface of the water layer do not have any effect on the processes responsible for surface modification, using computationally tractable sizes of the TTM-MD and CG MD parts of the model.

The thermophysical properties of Cr entering the TTM equations are as follows. The electron heat capacity of Cr is approximated as $C_e = \gamma T_e$ with $\gamma = 194 \text{ J m}^{-3} \text{ K}^{-2}$.⁷¹ Constant values of the electron–phonon coupling factor, $G = 4.2 \times 10^{17} \text{ W m}^{-3} \text{ K}^{-1}$,⁷² and the lattice heat capacity, $C_l = 3.23 \times 10^6 \text{ J m}^{-3} \text{ K}^{-1}$,⁷³ are assumed in the simulation. The temperature dependence of the electron thermal conductivity is approximated using the Drude model relationship, $K_e(T_e, T_l) = v^2 C_e(T_e) \tau_e(T_e, T_l)/3$, where $C_e(T_e)$ is the electron heat capacity, v^2 is the mean square velocity of the electrons contributing to the

electron heat conductivity, approximated as the Fermi velocity squared, v_F^2 , and $\tau_e(T_e, T_l)$ is the total electron scattering time defined by the electron–electron scattering rate, $1/\tau_{e-e} = AT_e^2$, and the electron–phonon scattering rate, $1/\tau_{e-ph} = BT_l$, so that $1/\tau_e = AT_e^2 + BT_l$. The value of the coefficient $A = 2.66 \times 10^6 \text{ K}^{-2} \text{ s}^{-1}$ is estimated with the free electron model,⁷⁴ while the coefficient B is described as a function of the lattice temperature and the phase state of the material, so that the experimental temperature dependence of thermal conductivity of Cr under conditions of electron–phonon equilibrium⁷⁵ is reproduced for both solid and liquid states. In particular, this description accounts for the two-fold drop of thermal conductivity as the temperature increases from 300 K to the melting point.

The laser irradiation is represented through a source term added to the TTM equation for the electron temperature.⁶² The source term has a temporal Gaussian profile corresponding to a 200 fs pulse and accounts for the exponential attenuation of the deposited laser energy with depth. The optical absorption depth of Cr is equal to 9.6 nm at a wavelength of 258 nm.⁴⁵ The absorbed laser fluence is spatially modulated along the x -direction to represent the periodic absorption pattern generated by the interference of the incident laser wave and surface scattered electromagnetic waves responsible for the LIPSS formation.^{15,16} We note that, in a more controlled manner, the spatial modulation of the laser energy deposition can be achieved through interference between multiple laser beams focused on the same laser spot.^{7,13,14} The period of the sinusoidal modulation is 260 nm, which matches the size of the computational cell in the x -direction. The minimum and maximum local absorbed fluences are 2000 to 3000 J m^{-2} , which correspond to 20% modulation of the laser energy deposition with respect to the average level of 2500 J m^{-2} . This average fluence is more than 60% above the phase explosion threshold of 1500 J m^{-2} established in a series of small-scale simulations of 200 fs laser pulse irradiation of Cr under vacuum. Before applying the laser irradiation, the whole system shown in Fig. 8 is thermalized at 300 K for 300 ps.

Experimental setup

The experiments are performed in a single pulse laser ablation irradiation regime for a single crystal Cr target with a (001) surface orientation, *i.e.*, for conditions similar to those studied computationally. The laser irradiation was performed with an Yb:KGW laser source emitting linearly polarized pulses with a pulse duration of 200 fs, a 1 kHz repetition rate, and a 1026 nm central wavelength. The experimental setup shown in Fig. 9 also includes a system of a half-waveplate (HW) and a linear polarizer (LP) used to adjust the laser power, a dichroic mirror (DM) to guide the beam, a plano-convex lens (CL) with a focal distance of 200 mm to focus the beam onto the sample, and a CMOS camera to observe the sample surface. The sample was placed in a small cell filled with distilled water covering the surface of the sample and up to 0.5 mm above. Then,

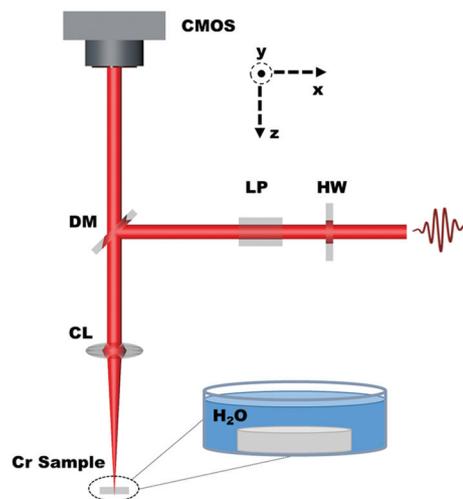


Fig. 9 Illustration of the experimental setup for the irradiation of a Cr sample submerged in water.

the cell was set on a computer controlled 3-axis translational stage. The spot size was measured and calculated to be $\sim 32 \mu\text{m}$ in diameter at $1/e^2$ using a CCD camera on the focal plane within the lens Rayleigh range. The incident laser fluence of individual laser pulses is estimated to be 6000 J m^{-2} for irradiation in both air and water environments. In all experiments, the normal direction of laser incidence with S-polarization with respect to the sample surface was used. The morphology of the laser-induced structures was analyzed using JEOL JSM-7500F SEM and FEI 80-300 kV Titan TEM/STEM microscopes.

Conflicts of interest

There are no conflicts to declare.

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